



NSTAR

**JPL**

Ion Propulsion Validation on DS1

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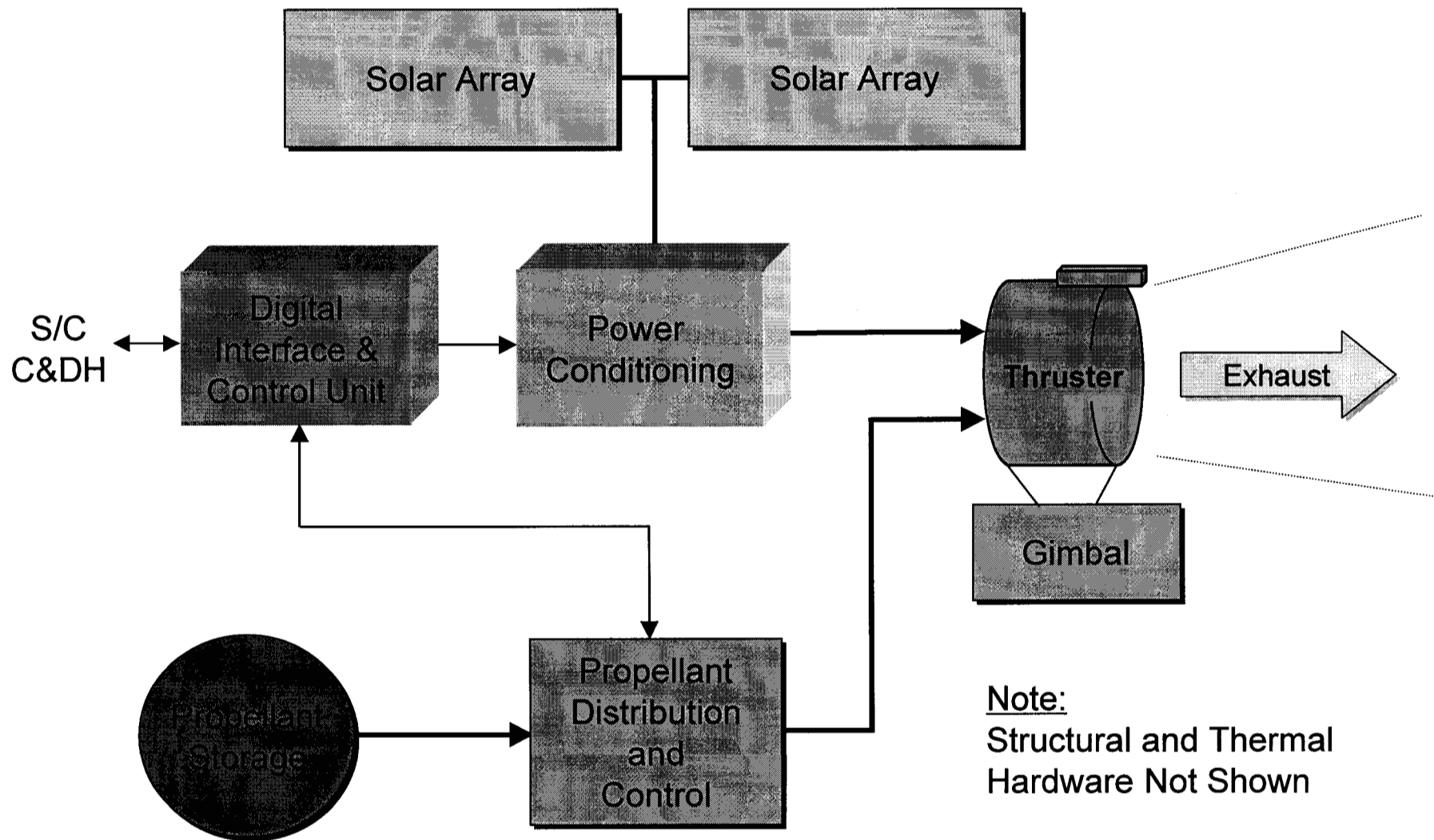
NSTAR Technology Validation Goals

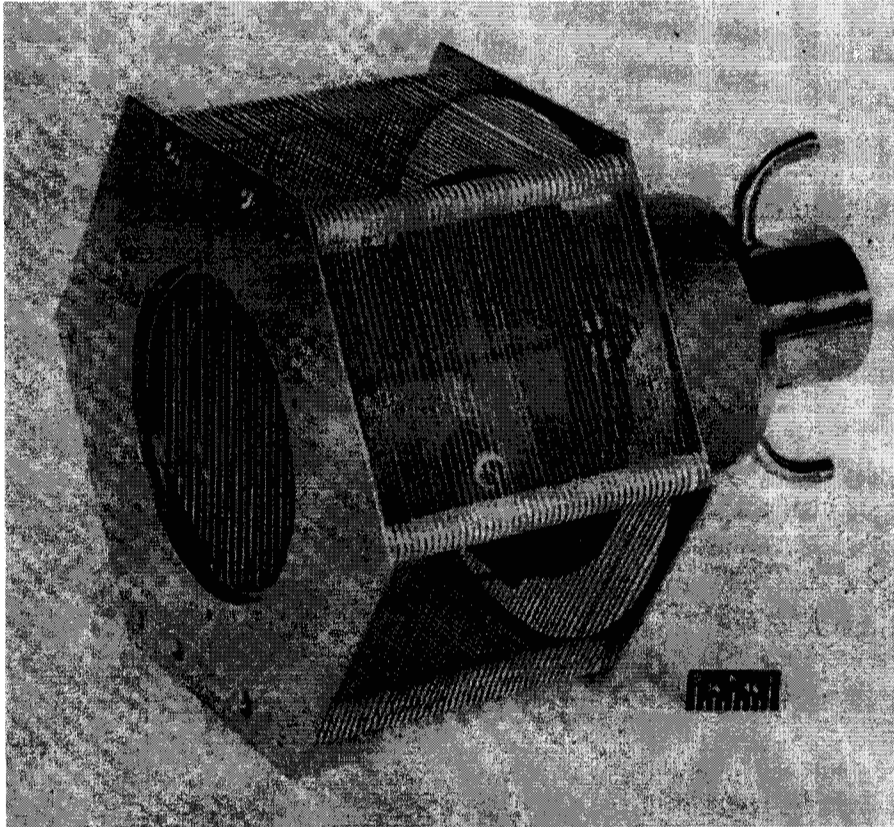


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- ① **Demonstrate that the NSTAR 30-cm diameter ion engine had sufficient life to perform missions of near-term interest -- *No one had ever successfully operated an ion engine intended for primary propulsion for its full design life***

- ② **Demonstrate through a flight test that the ion propulsion system hardware and software could be flight qualified and successfully operated in space, and demonstrate control and navigation of an SEP spacecraft**





- **1957:** An experimental research program in electric propulsion is initiated at Lewis Flight Laboratory
- **1959:** JPL forms a study group for electric propulsion systems
- **1959:** The first electron-bombardment ion thruster is successfully operated in the laboratory at Lewis Research Center by **Harold Kaufman**
- The performance is excellent
 - ♦ $I_{sp} = 5000s$
 - ♦ efficiency > 60%



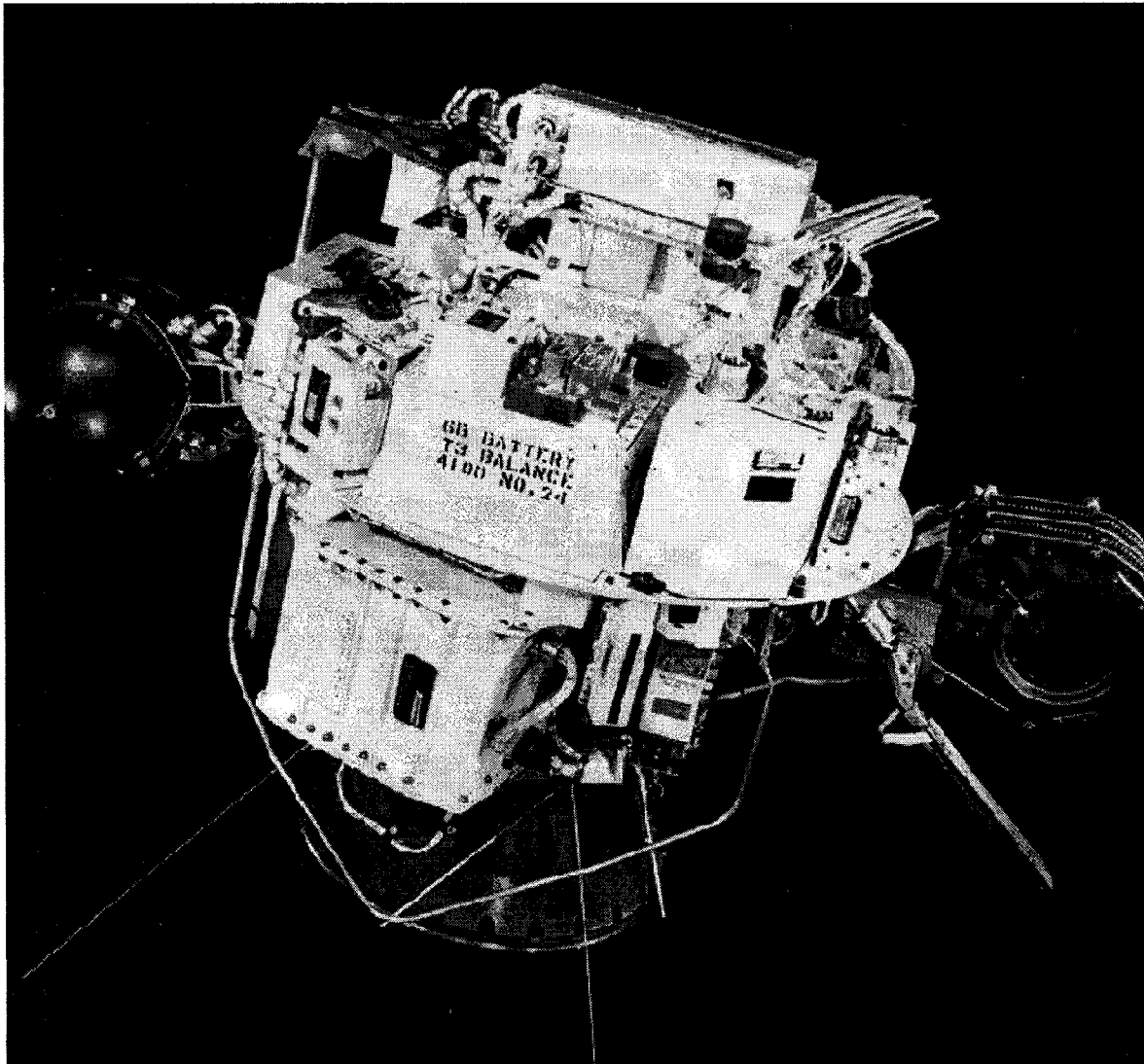
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1964 -- SERT I

Space Electric Rocket Test 1

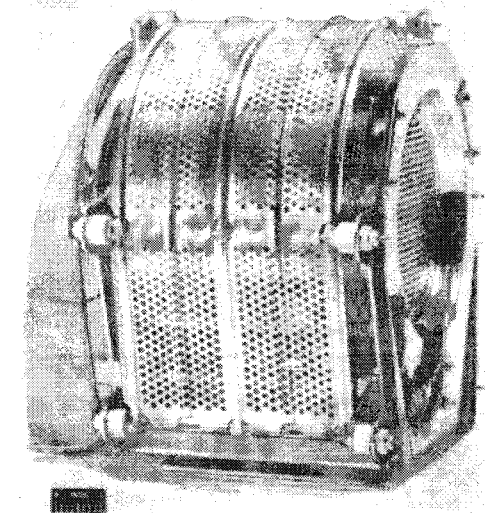


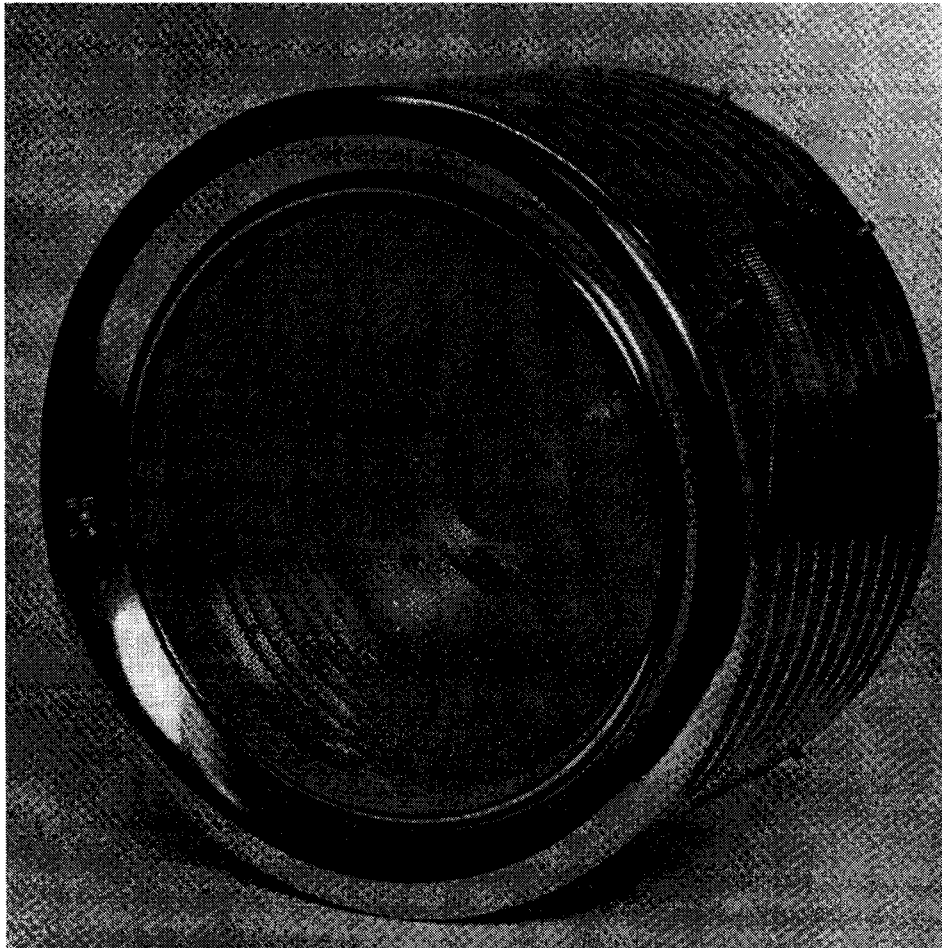
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***“Does she or
Doesn’t she?”***

“She Does!”



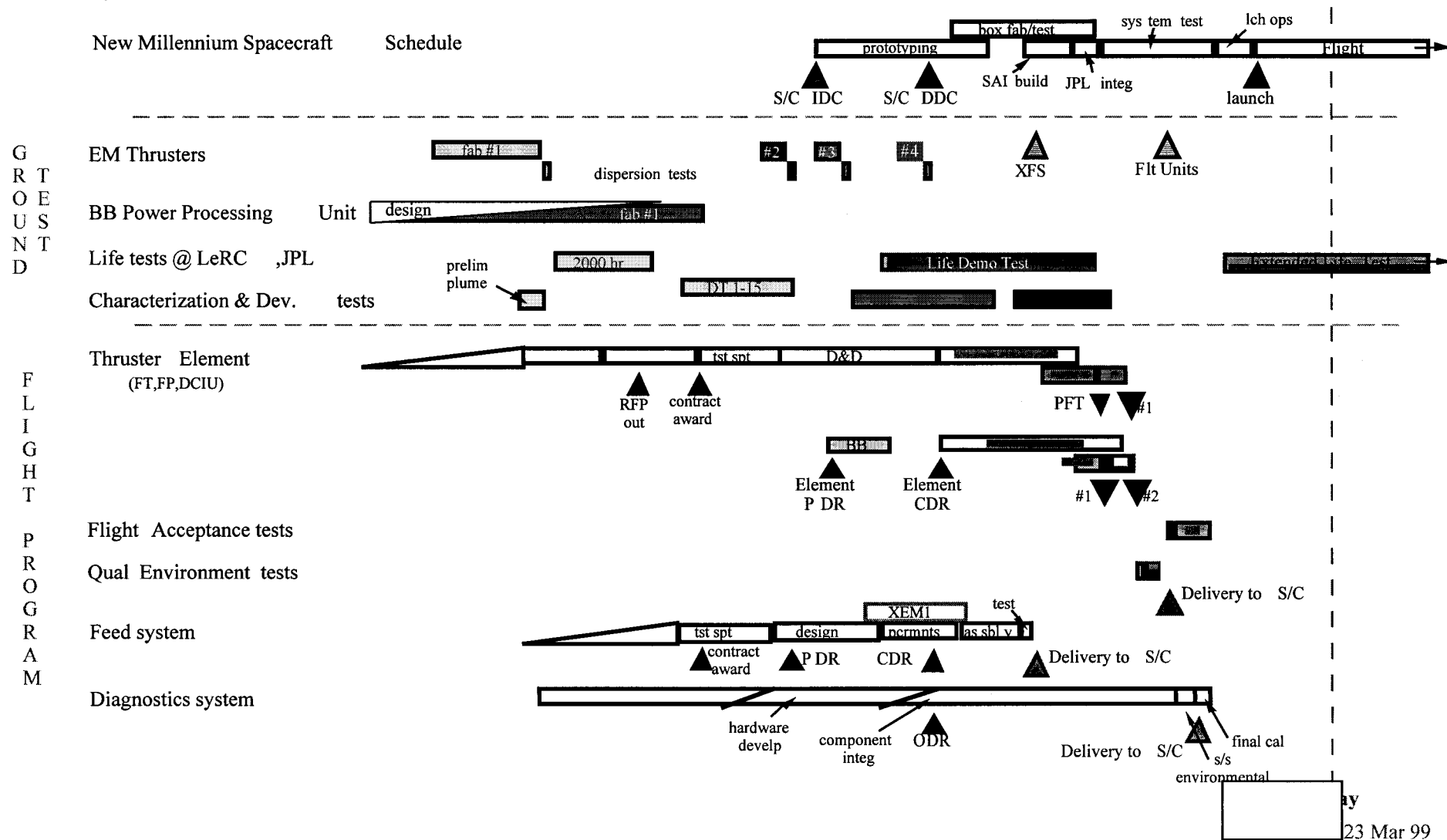


1970: Hughes-Built 30-cm Ion Engine

- **Started in 1970**
- **100 series though 900 series then J-Series (i.e., 1000 series)**
- **Major Innovation: Dished Grids (which are essentially the same as those flying on DS1)**
- ***Always life test thruster with serial #1***

AT - Acceptance Test
 FT - flight thruster
 FP - flight PPU
 functional integrations

CY93	CY94	CY95	CY96	CY97	CY98	CY99
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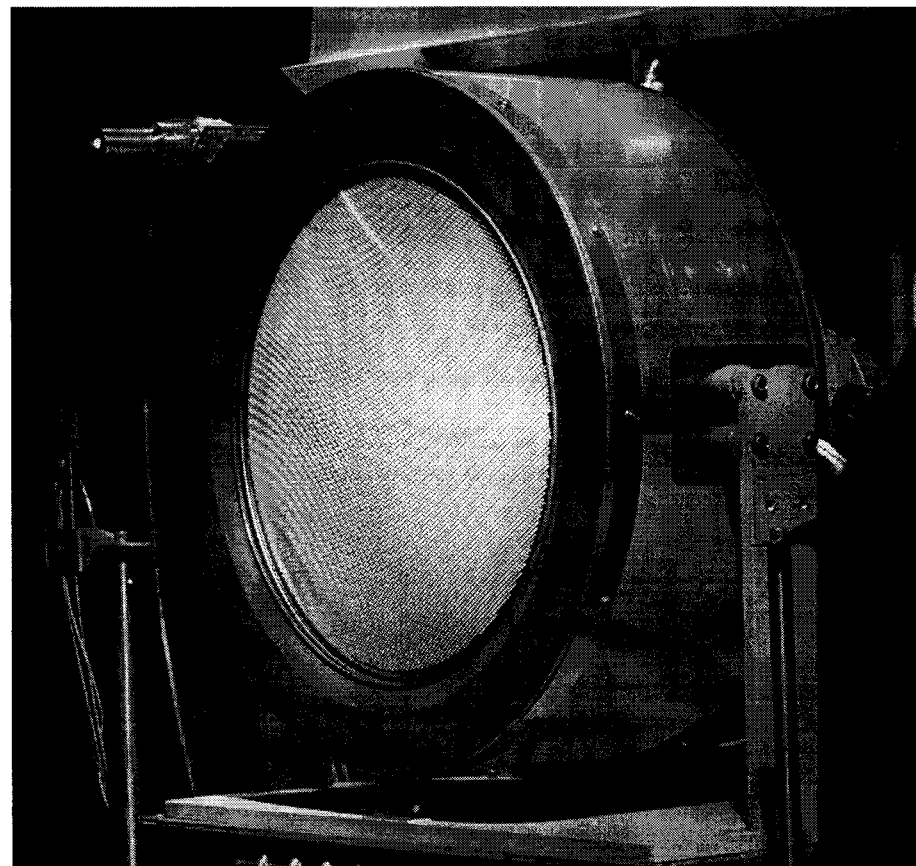
-
- ⑩ Cathode heater failure due to thermal cycling
 - ⑨ Erosion of the neutralizer orifice plate due to plume mode operation
 - ⑧ Structural failure of the screen grid due to ion sputtering
 - ⑦ Structural failure of the keeper orifice plate due to ion sputtering
 - ⑥ Structural failure of the accelerator grid or electron-backstreaming due to rogue hole formation
 - ⑤ Unclearable short between the cathode and the keeper electrode
 - ④ Depletion of cathode low-work-function material
 - ③ Unclearable short between the screen and accelerator grids
 - ② Structural failure of the accelerator grid by charge-exchange ion erosion
 - ① Electron-backstreaming due to enlargement of the accelerator grid apertures by ion sputtering

- **Goals**

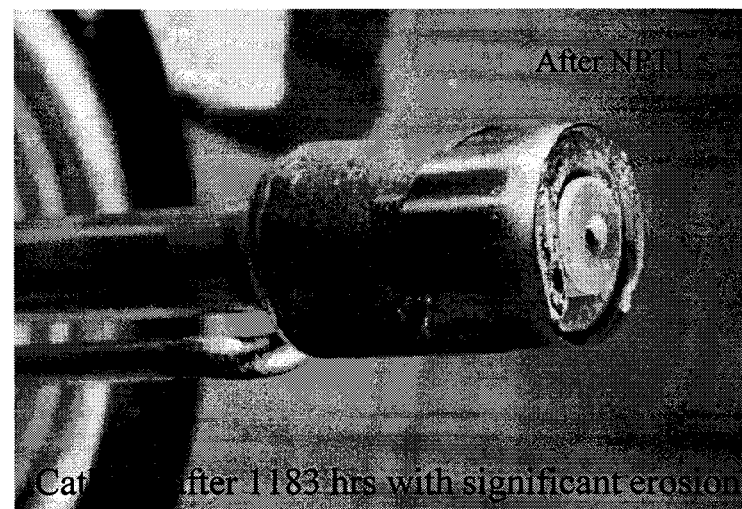
- ◆ 8,000 hrs at full power with Engineering Model thruster (82 kg xenon throughput)
- ◆ > 12,000 hrs at several thrust levels -- 125 kg xenon throughput with flight spare engine

- **Actual**

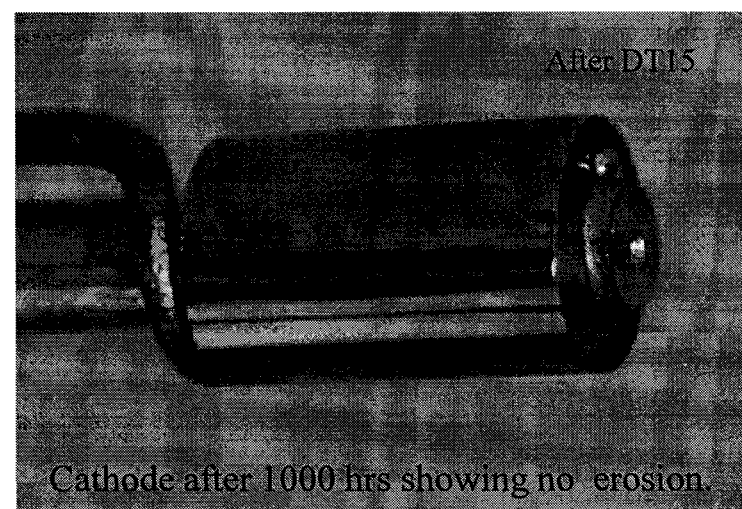
- ◆ 8,200 hrs at full power -- 88 kg throughput demonstrated
- ◆ 8,700 hrs with flight spare engine and counting -- 76 kg throughput demonstrated to date (as of 2/7/00)

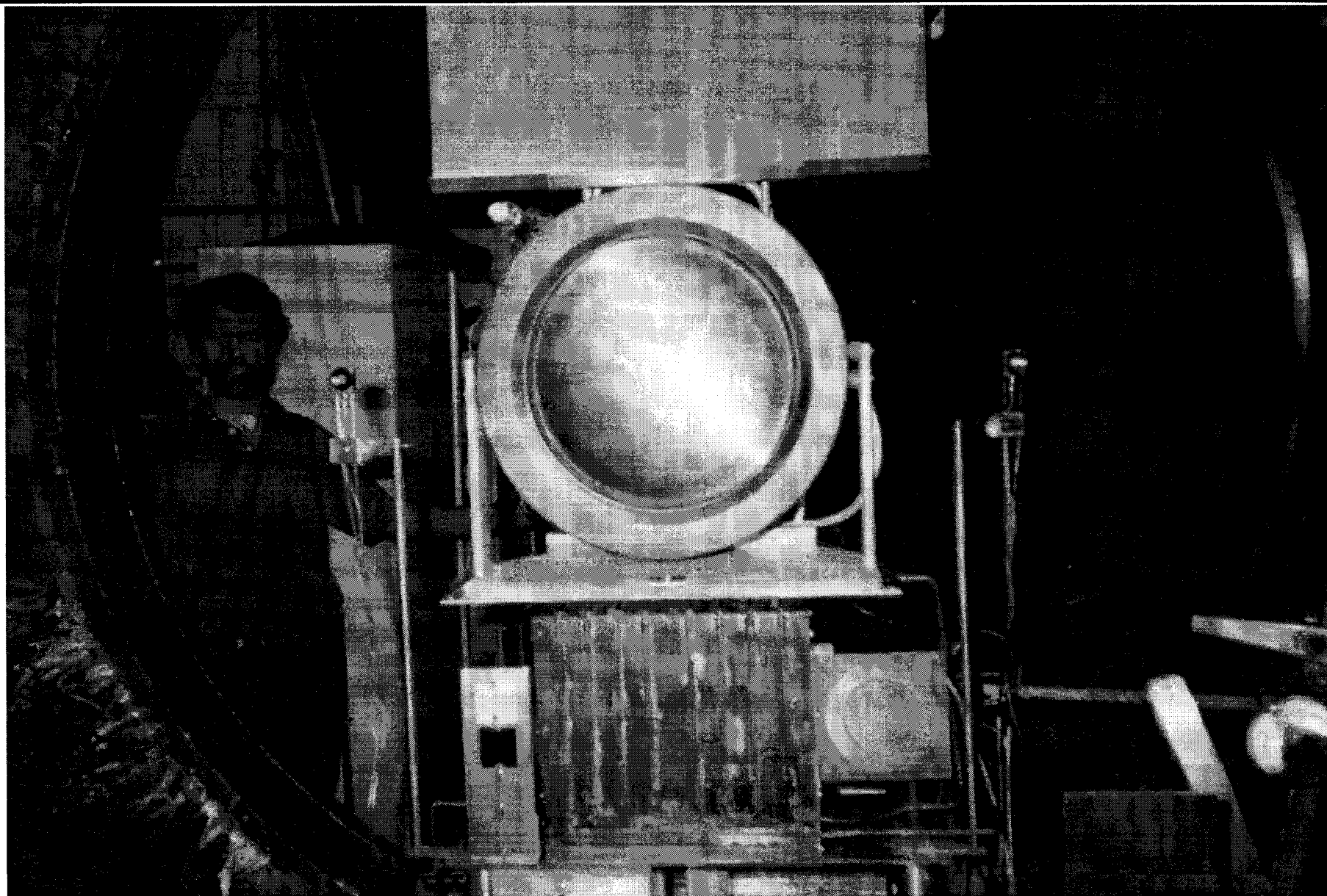


- Significant cathode erosion observed after only 1000 hrs

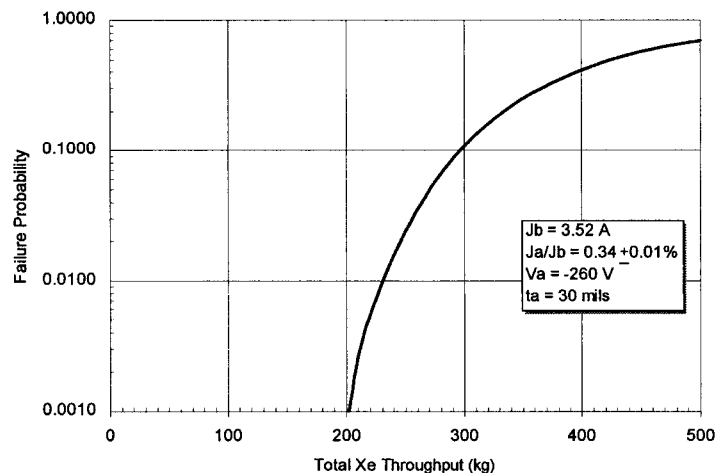
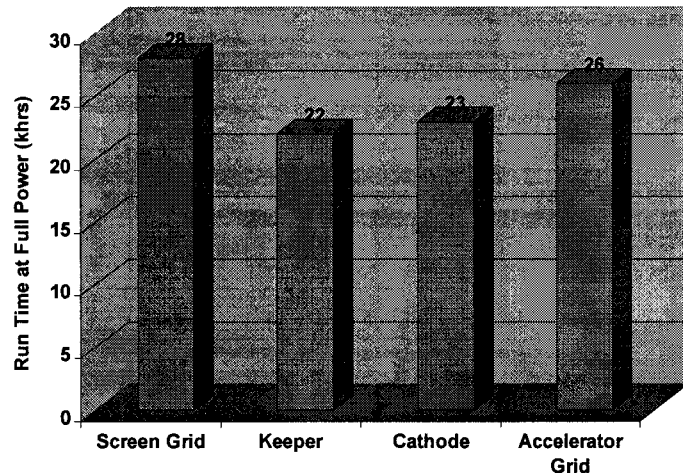


- Used an enclosed keeper configuration to eliminate cathode erosion



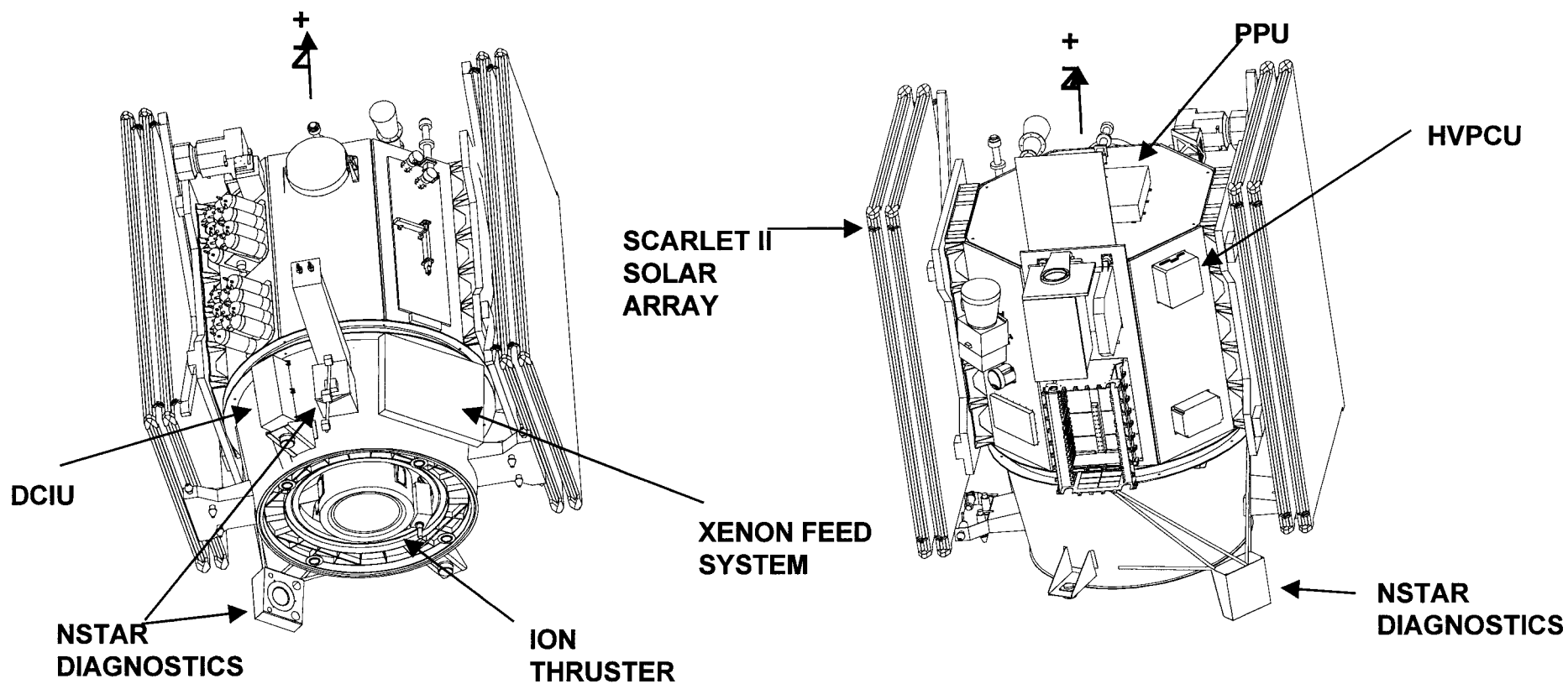


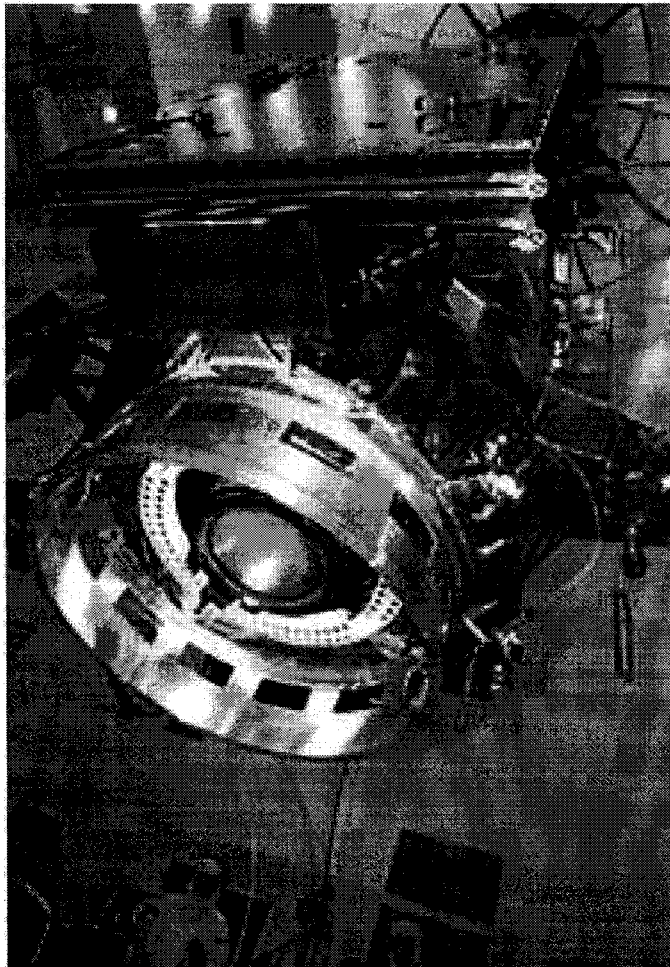
Approximate Failure Distribution Peaks



CONCLUSIONS

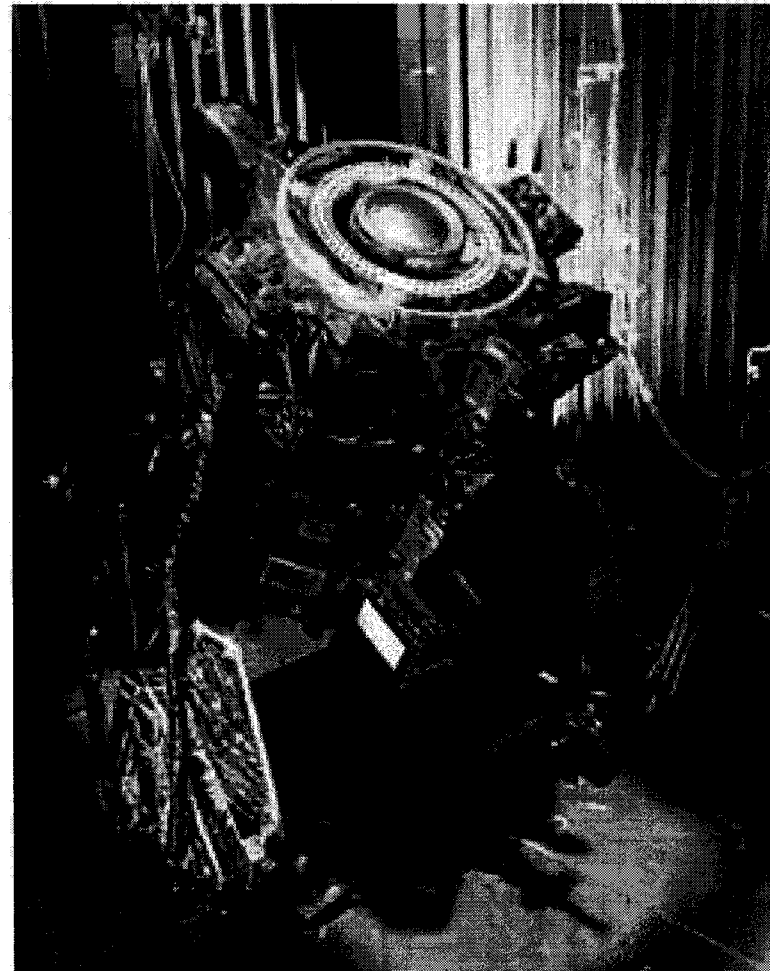
- Everything in the engine will fail at the same time
- Performing the ST4 mission with the 3-engine system currently baselined appears to be within the engine's throughput capability





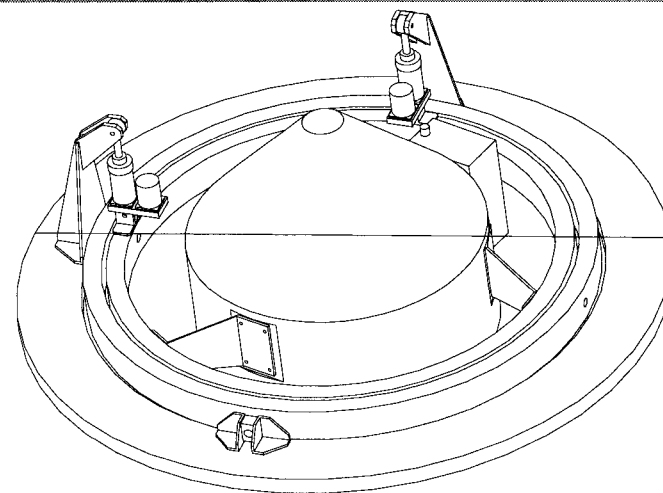
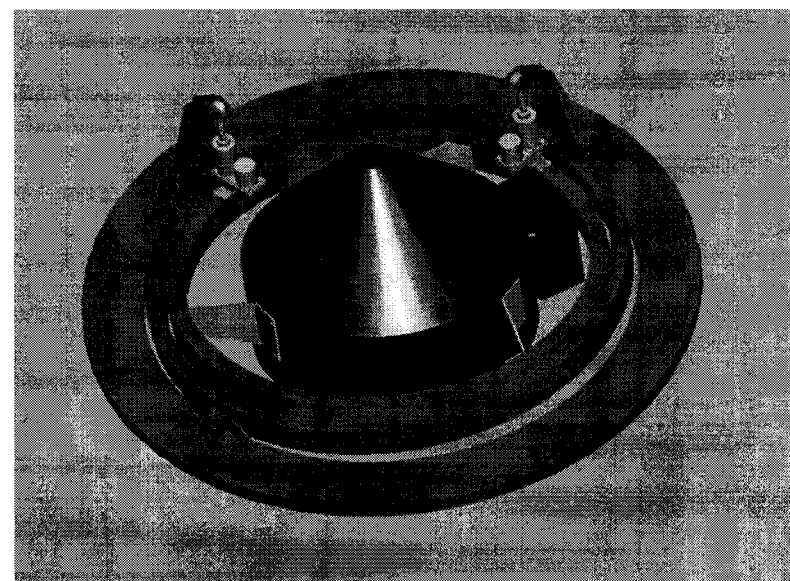
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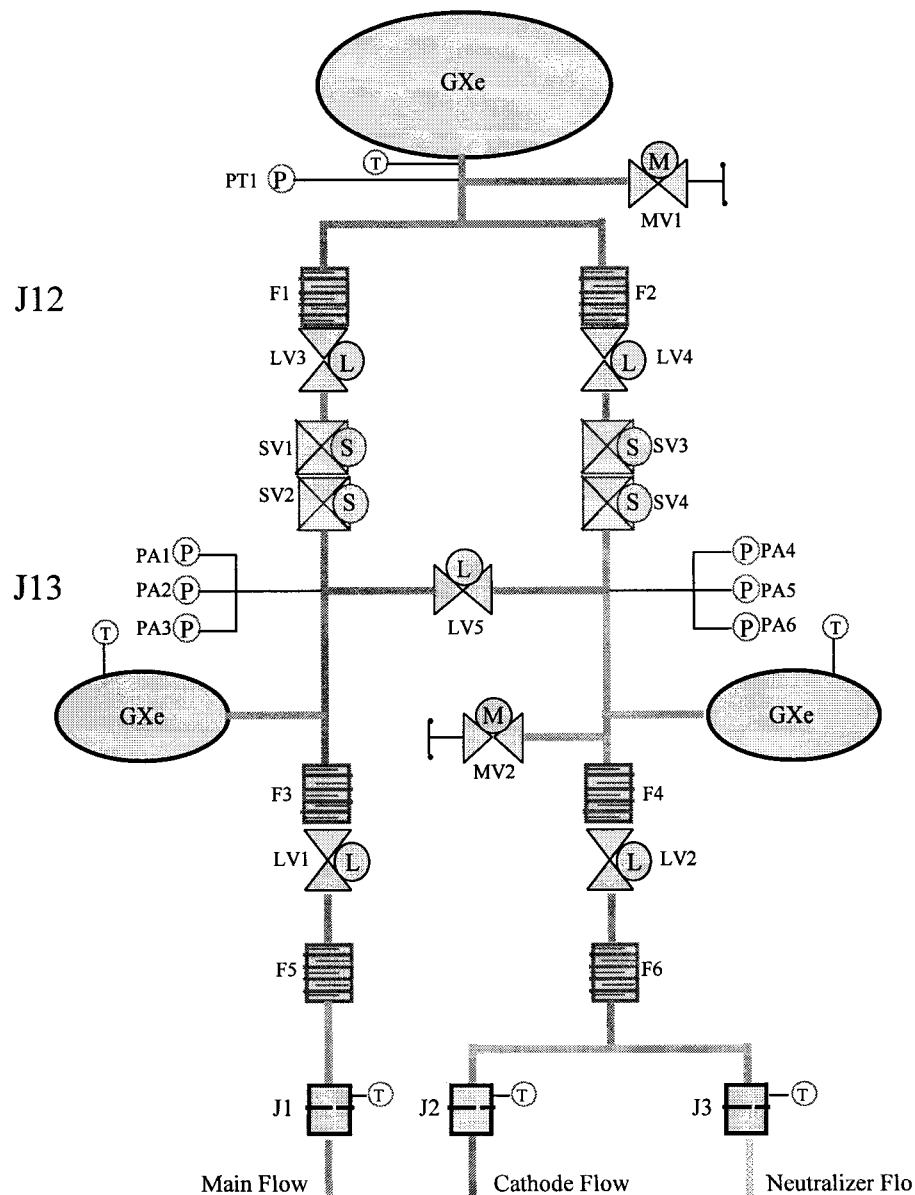
NASA/JPL/Caltech



NASA/JPL/Caltech

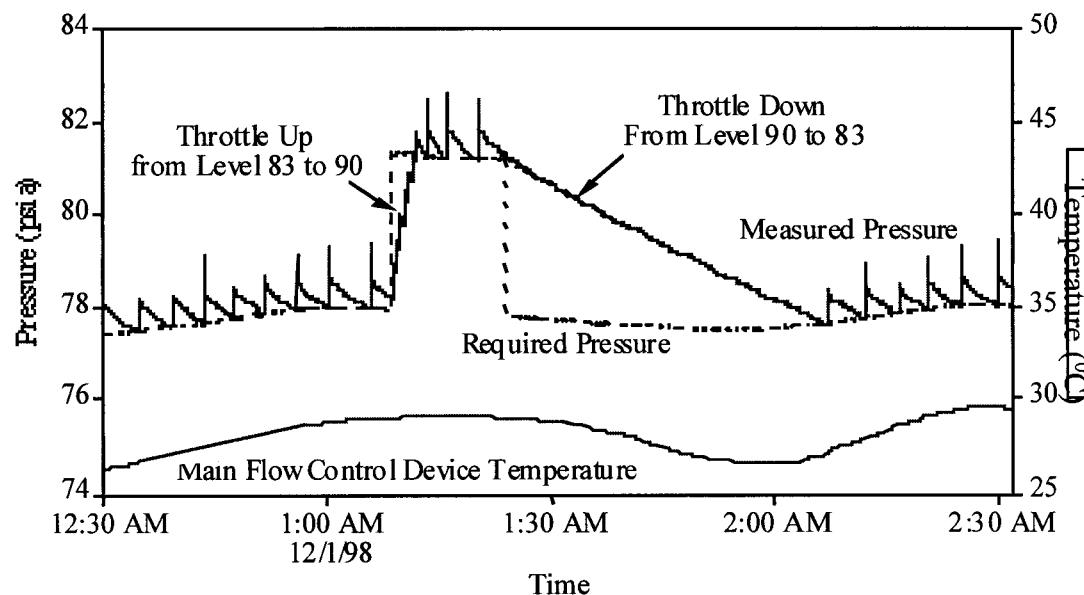
- **Two concentric mounting rings**
 - ◆ hollow aluminum channel
 - **Two linear actuators**
 - ◆ enable ± 5 deg in 2 dimensions
 - ◆ 1 mrad position accuracy
 - **Three flex brackets**
 - ◆ conductive isolation
 - ◆ titanium for stiffness
 - **Hardware pictured - 23.26 kg**
-
- **Shims used to align thrust vector with C.G.**
 - **Thermal cover not shown**
 - **Thruster - PPU cable is ~4.8 m long**
 - ◆ minimize length if possible





Xenon flow:

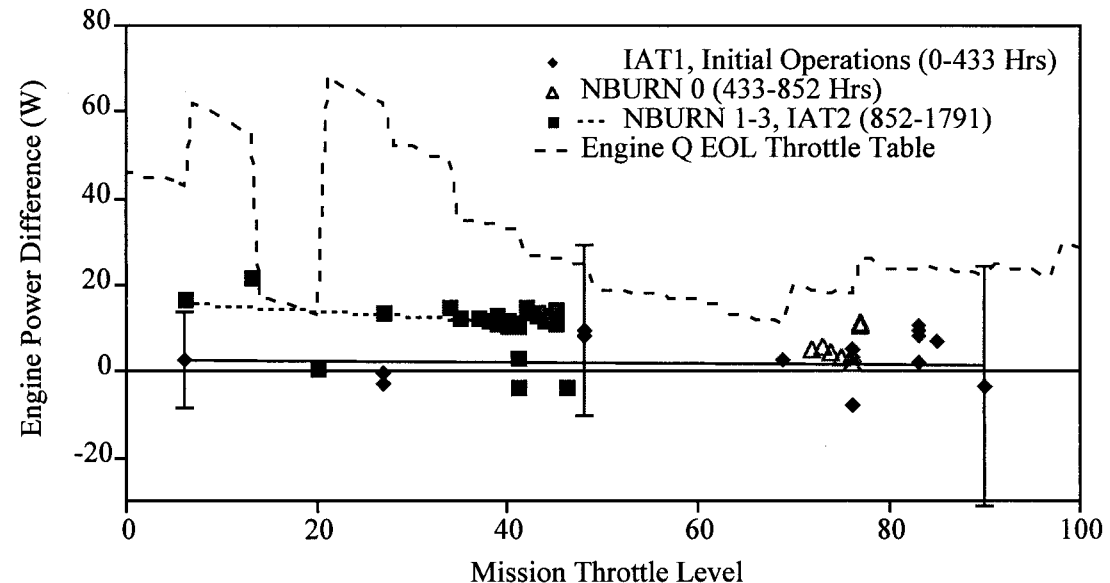
- **Main flow behavior during power increases and decreases is shown**
 - ◆ sawtooth magnitude dependent on main tank pressure
 - ◆ new power level selected determines the negative slope
 - ◆ shows operation is slightly rich
- **Effects most pronounced during start - can take 7 hours to bleed down**
 - ◆ cathodes always start at 3.6 sccm (maximum value)
- **Voting algorithm for pressure transducers is key to proper flow control**



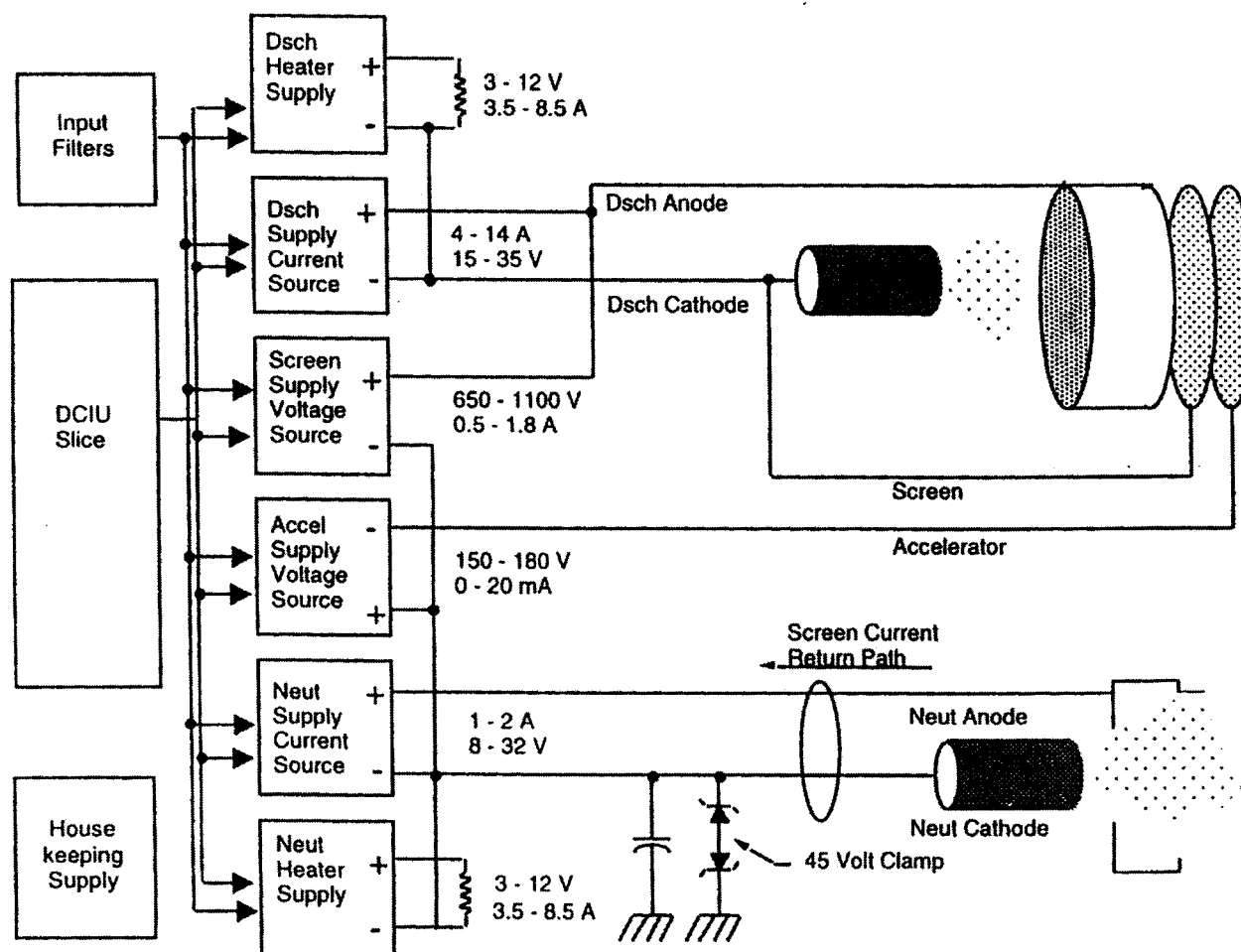
- **Initial design considered 1,2,3 plenum tanks**
- **Variable set point regulator is needed**
 - ✓ NSTAR: 2-30 sccm xenon
 - ✓ low flows need to be stable

Power and Thrust:

- **Doppler measurements within 0.5 mN**
 - ♦ team can identify the initiation of xenon flow before cathode start
- **$T = f(J_b, V_b, V_g, M_{xe}, e)$**
- **Expected values were from test data**



- **Ideal: symbols on 0 line**
- **Actual: | initial power levels close**
| later power levels are high
- **Cannot recheck initial levels yet**
- **Today's question: does the thruster behave differently in flight, was the ground data biased low, or is differing PPU efficiency introducing the variation?**



- ❖ **Ground test program more extensive than the original plan**
 - ◆ 13780 total test hours on 5 EM thrusters
 - ◆ direct contributor to 7800+ flight thruster hours (increasing by -300 hrs/week)
- ❖ **EMs proved invaluable**
 - ◆ development test costs were low
 - ◆ equipment handling practices and purge procedures were documented
 - ◆ diode mode proven with no risk to flight units
 - ◆ substitutions in system test enabled schedule to be preserved
- ❖ **Hardware proved to be interchangeable**
 - ◆ telemetry calibrations virtually the same for both PPUs
 - ◆ need to be conscientious about location of sense measurements & cable lengths
- ❖ **Original Project Plan did not include an end-to-end test (to save costs)**
 - ◆ risk eventually seen as too high for the savings
- ❖ **Flight data compares reasonably with expectations**
 - ◆ no interactions with plasma or optical instruments
 - ◆ diagnostics measurements detect many spacecraft events
 - ◆ operations are now routine

- **CNSR**
- **Venus Surface
Sample Return**
- **Europa Lander**
- **Titan Explorer**
- **Saturn Ring
Observer**
- **Neptune Orbiter**

